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APPLICATION  
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TITLE: ELECTRIC FIELD PROXIMITY DETECTOR FOR FLOATING AND  
GROUNDED TARGETS

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ELECTRIC FIELD PROXIMITY DETECTOR  
FOR FLOATING AND GROUNDED TARGETS

5 FIELD OF THE INVENTION:

The present invention relates to proximity detectors, and more particularly to proximity detectors that employ electric field sensing to detect physical objects.

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BACKGROUND OF THE INVENTION:

Electric field proximity detectors are well known. Various types of detectors have been documented which utilize electric fields to sense the presence of conductive or

15 partially conductive objects entering their effective field of detection. Generally, objects are detected by measuring signal changes resulting from perturbations in a generated electric field. Electric field proximity detectors are advantageous in that they are generally safe, fast, inexpensive, and capable of measuring object distance to a high degree of resolution.

20 One specific variety of electric field sensing proximity detector is the so-called transmit-receive type. In a typical configuration, this variety of detector generates a low-frequency electric field at one transmitting electrode and detects the electric field at a second receiving electrode. Intruding objects affect the degree of capacitive coupling between the transmitting electrode and receiving electrode, and as a result their presence 25 may be detected by measuring changes in the signal at the receiving electrode.

Known transmit-receive detectors operate predominantly in two modes. The first, or transmitter, mode is triggered when objects with high impedance to circuit ground (that is, electrically floating objects) enter the generated electric field. In this mode, the floating 30 object behaves essentially as a conductive extension of the transmitting electrode. Electrical charge from the generated electric field travels along the object towards the receiving electrode more efficiently than it does through free space, and as a result, the capacitive

coupling between the transmitting electrode and the receiving electrode increases. Accordingly, the signal at the receiving electrode also increases, and the proximity of the floating object is thereby indicated. (The foregoing assumes that the floating object is not so large as to behave like an earth-grounded object.)

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The second, or shunt, mode is triggered when objects with low impedance to circuit ground (that is, objects grounded to circuit ground) enter the generated electric field. In this mode, the capacitive coupling between the transmitting electrode and the receiving electrode decreases as the grounded object draws near because the intruding object 10 effectively shunts the intercepted electric field to circuit ground. Accordingly, the signal at the receiving electrode decreases as the object approaches, and the proximity of the grounded object is thereby indicated.

— The existence of two separate modes of operation in known transmit-receive proximity detectors as described has two notable disadvantages. The first drawback is the added complexity in detector circuitry that is required to detect both floating and grounded objects. Because floating objects trigger an increase in current at the receiving electrode whereas grounded objects trigger a decrease in current, detector circuitry must be capable of detecting both of these types of signal changes. This requirement may add to the 20 complexity of detector circuitry, especially if the device is intended to be capable of distinguishing between floating versus grounded objects.

The second and more serious drawback of the two operating modes of known detectors is the resulting inability of these devices to reliably sense objects with intermediate degrees of ground impedance. Again, because objects with high impedance to earth ground trigger an increase in current at the receiving electrode whereas objects with low impedance to circuit ground trigger a decrease in current, it follows that, for certain 25 objects with intermediate impedance to circuit ground, no perceptible change in current will occur at the receiving electrode. Objects having such a degree of ground impedance may therefore, disadvantageously, escape detection. As a result, known transmit-receive 30 proximity detectors are poorly suited for many safety applications.

Still another drawback of known transmit-receive type detectors is their susceptibility to stray capacitance. Component circuitry associated with the transmission and detection of the electric field in these devices may emit stray electric fields and capacitances that influence the measured signal at the receiving electrode. As a result, this  
5 stray capacitance may jeopardize proper object detection.

Hence what is needed is a transmit-receive type electric field proximity detector that is capable of reliably detecting objects, regardless of their impedance to circuit ground, that additionally has a reduced susceptibility to the corrupting effect of stray capacitance, and  
10 that optimally provides a single characteristic signal change for all detected objects.

#### SUMMARY OF THE INVENTION:

15 It is an object of the present invention to provide a transmit-receive type electric field proximity detector which permits objects to be reliably detected regardless of their impedance to circuit ground.

20 The present invention may also provide a transmit-receive type electric field proximity sensor with reduced susceptibility to stray capacitance.

25 The present invention may further provide a transmit-receive type electric proximity detector suitable for use in safety applications, such as the automatic switching of a portable or cellular telephone from loudspeaker mode to handset mode when the handset is brought close to the user's ear, for example.

Briefly, in the present invention, at least one circuit ground electrode is used in addition to the traditional transmitting and receiving electrodes. The circuit ground electrode, transmitting electrode and receiving electrode are sized and arranged such that, as  
30 a target object draws near, there is a prevailing decrease in the current at the receiving electrode (at least outside a threshold distance) upon the intrusion of any conductive or partially conductive object, regardless of its impedance to earth ground.

In addition, the positioning of the ground electrode with respect to the detector circuitry may be such that the sensing electrodes are effectively shielded from the stray electric fields and capacitances that may be induced by component circuitry within the 5 device. This results in reduced susceptibility to stray capacitance.

In accordance with one aspect of the present invention, there is provided a transmit-receive type electric field proximity detector suitable for detecting partially conductive or conductive objects regardless of their impedance to circuit ground, said detector 10 comprising: a transmitting electrode; a receiving electrode; and at least one ground electrode, arranged and sized such that, upon the approach of an object, a signal received by said receiving electrode decreases, at least until said object is within a threshold distance of one of said transmitting electrode, receiving electrode, and at least one ground electrode.

15 In accordance with another aspect of the present invention, there is provided a sensor suitable for use in a transmit-receive type electric field proximity detector, said sensor having a circuit ground and comprising: a transmitting electrode; a receiving electrode; and at least one circuit ground electrode, arranged and sized such that, upon the approach of an object, the effective impedance between the receiver electrode and the at 20 least one circuit ground electrode decreases more quickly than the sum of the impedance between the receiver electrode and the at least one circuit ground electrode and the impedance between the transmitting electrode and the receiving electrode, at least until said object is within a threshold distance of one of said transmitting electrode, receiving electrode, and at least one ground electrode.

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In accordance with yet another aspect of the present invention, there is provided a communications device comprising:

30 (a) a transmit-receive type electric field proximity detector suitable for detecting partially conductive or conductive objects regardless of their impedance to circuit ground, said detector comprising:  
a transmitting electrode;

a receiving electrode; and

at least one ground electrode,

arranged and sized such that, upon the approach of an object, the effective impedance between the receiver electrode and the at least one circuit ground electrode decreases more quickly than the sum of the impedance between the receiver electrode and the at least one circuit ground electrode and the impedance between the transmitting electrode and the receiving electrode, at least until said object is within a threshold distance of one of said transmitting electrode, receiving electrode, and at least one ground electrode,

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said detector further comprising detector circuitry coupled to said receiving electrode and being responsive to the induced electrical signal therefrom for generating an output signal indicative of the approach of an intruding object; and

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(b) a switch capable of switching between a receiver mode and a loudspeaker mode;

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said output signal of said proximity detector being coupled to said switch to operate said communications device in loudspeaker mode when said device is separated by at least a predetermined threshold distance from a user's ear and in the receiver mode when said device is separated by less than said predetermined threshold distance from the user's ear.

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In accordance with a further aspect of the invention, there is provided a sensor suitable for use in a transmit-receive type electric field proximity detector, said sensor having a circuit ground and comprising: a transmitting electrode driven with a low impedance; a receiving electrode actively held at circuit ground potential; and at least one circuit ground electrode connected to an earth ground, arranged and sized such that, upon the approach of an object, the capacitance between the object and circuit ground increases more quickly than the product of the capacitance between the object and the transmitting electrode and the capacitance between the object and the receiving electrode, at least until

said object is within a threshold distance of one of said transmitting electrode, receiving electrode, and at least one ground electrode.

Other aspects and features of the present invention will become apparent to those  
5 ordinarily skilled in the art upon review of the following description of specific  
embodiments of the invention in conjunction with the accompanying figures.

#### BRIEF DESCRIPTION OF THE DRAWINGS:

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In figures which illustrate, by way of example, embodiments of the present  
invention,

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FIG. 1 is a schematic diagram illustrating an electric field proximity detector  
exemplary of an embodiment of the present invention;

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FIG. 2A is a perspective view of a sensor configuration in accordance with FIG. 1;

FIG. 2B is a cross-sectional view from the side along the line 2B-2B of FIG. 2A;

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FIG. 3 is a schematic diagram illustrating the relevant capacitances existing in the  
embodiment of FIG. 1 as an object is sensed;

FIG. 3A is a Thevenin equivalent of the diagram of FIG. 3;

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FIG. 3B is a simplified diagram following from the diagram of FIG. 3 given certain  
assumptions;

FIG. 4A is a schematic diagram illustrating the electrical field associated with the  
embodiment of FIG. 1 sensing an object with low impedance to earth ground;

FIG. 4B is a graph illustrating the relationship between receiver current and the object-to-electrode distance of an object with low impedance to earth ground in the embodiment of FIG. 1;

5 FIG. 5A is a schematic diagram illustrating the electrical field associated with the embodiment of FIG. 1 sensing an object with high impedance to earth ground;

10 FIG. 5B is a graph illustrating the relationship between receiver current and the object-to-electrode distance of an object with intermediate or high impedance to earth ground in the embodiment of FIG. 1;

15 FIG. 6 is a schematic diagram of a system incorporating the detector of FIG. 1 with the sensor configuration of FIG. 2A; and

15 FIG. 7 is a perspective view of an alternative sensor configuration in accordance with FIG. 1;

20 DETAILED DESCRIPTION:

With reference to the schematic diagram of FIG. 1, a proximity detector 10 has a sensor 20 coupled to a detector body 28. The sensor 20 comprises a transmitting electrode 12, a receiving electrode 14, a first ground electrode 32 and a second ground electrode 16. The ground electrodes 32 and 16 are electrically coupled to one another but are electrically insulated from both the transmitting electrode 12 and the receiving electrode 14. The actual position and sizing of the electrodes is described hereinafter.

Detector body 28 houses electronic circuitry including an oscillator 18, an amplifier 22, and preferably, a signal detector 24. The oscillator 18 consists of a low-frequency alternating current ("AC") signal generator. The output of oscillator 18 is electrically coupled to the transmitting electrode 12. The ground electrodes 32 and 16 are electrically coupled to the circuit ground 70 of the detector circuitry. It should be noted that circuit

ground 70 may in fact be distinct from earth ground. The receiving electrode, amplifier, and signal detector circuitry are electrically coupled in series, such that the receiving electrode 14 is coupled to the input of the amplifier 22, and the output of the amplifier 22 is coupled to the input of the signal detector 24.

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The proximity detector 10 generates an electric field from the transmitting electrode 12 and detects an electric field 44 at the receiving electrode 14. The generated field is a low-frequency field with a wavelength  $\lambda$  much larger (at least 10 times greater) than the characteristic size of the system (the system now including the distance to the object) as 10 defined hereinbefore, with larger wavelengths being preferable. An embodiment with the object being up to 10 cm distant may therefore have a frequency up to about 300 kHz. To achieve an acceptable signal-to-noise ratio, the lower bound on the frequency is about 10 kHz.

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Sensor 20 is oriented and positioned in relation to the detector circuitry such that the ground electrode 16 is interposed between the detector circuitry and the "active" electrodes, namely, the transmitting and receiving electrodes 12 and 14.

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FIGS. 2A and 2B illustrates an exemplary configuration for the sensor 20 of FIG. 1. Referring to FIGS. 2A and 2B, the electrodes of the sensor 220 lie in two generally parallel planes, with the transmitting, receiving and first ground electrodes 212, 214 and 232, respectively, lying in a front plane in a "bulls-eye" configuration, and the second ground electrode 216 occupying a back plane behind the other electrodes.

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The transmitting electrode 212 consists of a generally circular disk of conductive material, forming the center of the "bulls-eye" configuration. The receiving electrode 214 is a circular annular ring of conductive material and surrounds transmitting electrode 212. The ground electrode 232, which is also a generally circular annular ring of conductive material, is interposed between the central transmitting electrode 212 and the surrounding 30 receiving electrode 214. The three electrodes in the front plane are nested concentrically about a common center line and are spaced from one another. More specifically, the ground electrode 232 has an outer diameter less than the inner diameter of the surrounding

receiving electrode 214, and an inner diameter greater than the diameter of the central transmitting electrode 212.

In the back plane, the ground electrode 216 is a generally circular plate of  
5 conductive material with a diameter approximately equal to the outer diameter of the outermost receiving electrode 214. The ground electrode 216 in the back plane is electrically coupled to ground electrode 232, however, both electrodes 232 and 216 are electrically insulated from the transmitting electrode 212 and the receiving electrode by a non-conductive material, such as rubber or air for example.

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The relative proportions of the front plane electrodes may be as set out in Table I below. With reference to FIG. 2B, 'tx' is the radius of the central transmitting electrode 212, 'gnd1' is the inner diameter to outer diameter width of the annular ring ground electrode 232, and 'rcv' is the inner diameter to outer diameter width of the annular ring receiving electrode 214. The ranges of Table I are suitable for an approaching object with a relative radius of 55. It should be noted that these proportions are relative, rather than in fixed units.  
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Electrode Measurement	Range
tx	$0 < tx < 15$
gnd1	$0 < gnd1 < 15$
rcv	$5 < rcv < 25$

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Table I: Relative Proportions of Sensor Electrodes

Thus if, for example, the approaching object had a radius of 110mm, a suitable radius for the transmitter would be between 0 and 30mm, a suitable annular width for the  
25 front plane ground electrode would be between 0 and 30mm and a suitable annular width for the receiver would be between 10 and 50 mm.

When any one of the three front plane electrodes is sized at the small end of its range as set forth in Table I, the remaining two electrodes may generally exceed the maximum end of their corresponding ranges. This is reflected in the further exemplary relative ranges set out in Table II below, which again are based on an object with a relative size of 55.

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R of tx	$\Delta r$ of gnd1	$\Delta r$ of rcv
1	1	1-30
1	5	1-45
1	10	1-35
1	20	10-20
5	1	1-35
5	5	1-45
5	10	1-40
10	1	1-40
10	5	1-30
10	10	5-30
20	1	1-20
20	5	1-15

Table II: Relative Proportions of Sensor Electrodes

10 The thickness of the electrodes is much less (at least ten times smaller) than the characteristic size of the system (that is, the length of a side of a cube that completely, though just, encloses the entire sensor).

15 Spacing between electrodes in the front plane is at least as large as the thickness of the electrodes. Furthermore, spacing between the ground electrode 216 in the back plane and the electrodes of the front plane is much less (at least ten times smaller) than the characteristic size of the system as defined above.

In FIG. 3, capacitances governing the functionality of the detector are illustrated.  
20 The transmitting electrode 12 and receiving electrode 14 act as two electrodes of a capacitor, forming a capacitance  $C_{TR}$  between them. Moreover, the transmitting and receiving electrodes form capacitances  $C_{TG}$  and  $C_{RG}$ , respectively, with circuit ground (represented by ground plate 32) and  $C_{TE}$  and  $C_{RE}$ , respectively, with earth ground 75. The circuit ground also has a capacitance with earth ground:  $C_{GE}$ . An intruding object may also

function as a capacitor electrode. For example, an intruding object 58 acts as an electrode, forming capacitances  $C_{OT}$ ,  $C_{OG}$ , and  $C_{OR}$  with the transmitting, ground, and receiving electrodes 12, 32 and 14, respectively, as well as a capacitance  $C_{OE}$  with earth ground 75.

5 The capacitances indicated in FIG. 3 may be reduced to the Thevenin equivalent capacitances illustrated in FIG. 3A. The value of each equivalent capacitance,  $C_{TR}^E$ ,  $C_{TG}^E$ ,  $C_{RG}^E$ , will, of course, change as the object moves. However, the Thevenin equivalent shows that the ratio of the voltage at the receiver to that at the transmitter is as follows:

where each  $Z$  term is an impedance term such that  $Z = 1/j\omega C$  (with  $j$  being the square root of minus 1 and  $\omega$  the oscillator signal frequency). Equation (1) indicates that the voltage at the receiver will decrease as the object approaches if the impedance between the receiver and ground,  $Z_{RG}^E$ , decreases more quickly than the sum of the impedances between the receiver and ground and the transmitter and receiver,  $(Z_{RG}^E + Z_{TR}^E)$ . This results for the sensor configuration described in conjunction with figures 2A and 2B, at least until the object approaches to within a threshold distance.

20 For the case where (i) the receiver is actively held at ground potential, (ii) the transmitter is driven with a low impedance, and (iii) the circuit ground is connected to the earth ground, the diagram of figure 3 simplifies to that shown in figure 3B. The operation of the detector 10 is explained in the context of this simplified case. With reference to figure 3B, noting that the current into the receiver is that through  $C_{TR}$  and that through  $C_{OR}$ ,  
 25 and also  $I_{CTR} = j\omega V C_{TR}$  and  $I_{COR} = j\omega V_o C_{OR}$ , we have the following:

$$\frac{V_O}{V} = \frac{Z_{OR} \parallel Z_{OE} \parallel Z_{OG}}{Z_{OT} + Z_{OR} \parallel Z_{OE} \parallel Z_{OG}} = \frac{C_{OT}}{C_{OT} + C_{OR} + C_{OE} + C_{OG}}$$

This implies the induced current at the receiving electrode  $\mathbf{I}_R$  is defined by the equation

$$I_R = j \omega V \left| \frac{C_{OR} C_{OT}}{C_{TR} + \frac{C_{OR} + C_{OT} + C_{OG} + C_{OE}}{\sqrt{C_{OR} C_{OT}}}} \right| \dots \dots \dots \quad (2)$$

When no object is present within the effective sensing range of the detector, it will be appreciated that the numerator of the second parenthetical term, that is, the product of  $C_{OR}$  and  $C_{OT}$ , is zero. Therefore, the base current  $I_{R\text{ BASE}}$ , which represents the steady state receiver current when no intruding object is present, is defined by the equation

$$I_{R\text{ BASE}} = j \omega V C_{TR\text{ BASE}}$$

15 where  $C_{TR \text{ BASE}}$  represents the steady state capacitance between the transmitting and receiving electrodes when no object is present.

In FIG. 4A, however, an electrically grounded object 58G has entered the effective sensing range of the detector 10. Note that the electrically grounded status of the object 20 58G is represented by its connection to earth ground 75 through low impedance  $Z_{low}$  46. A low impedance is defined in this context as an impedance that is much less than the characteristic impedance of the system (i.e., the impedance between the object and a combination of all the sensor electrodes). Because the impedance  $Z$  of the approaching object 58G to circuit ground is low, the capacitance  $C_{OG}$  becomes very large by virtue of the 25 relationship

$$C_{OG} = \frac{1}{j\omega Z}$$

30 Therefore, provided  $C_{OG}$  remains much greater than  $C_{OR}$  and  $C_{OT}$ , equation (2) reduces to

Consequently, with a low impedance between the object and ground, the receiver current  $I_R$  can be approximated by equation (3). Thus, it will be observed that in the case of grounded objects, the receiver current is dependent upon the capacitive coupling  $C_{TR}$  5 between the transmitting electrode and the receiving electrode.

As the grounded object 58G approaches the sensor, it intercepts a portion 48 of the generated electric field 56. The interception of the electric field by the object 58G changes the shape of the electric field and causes a portion 48 of the electric field 56 to be shunted 10 away from the receiving electrode 14 to ground 70 through the impedance  $Z_{low}$  46. This in turn decreases the capacitive coupling  $C_{TR}$  from its base level  $C_{TR\ BASE}$ . Accordingly, and with reference to the equation (3), the current  $I_R$  at the receiving electrode 14 also decreases 15 from its base level  $I_{R\ BASE}$ . This decrease in current is then amplified by amplifier 22 (FIG. 1) and converted to a RMS (Root Mean Square) voltage value  $V_{out}$  by the signal detector 24.

Ultimately, the proximity of the object 58G is indicated by a decrease in the RMS voltage output  $V_{out}$  of the signal detector 24.

FIG. 4B illustrates the general relationship of object-to-electrode distance to the detector's DC output  $V_{out}$  when the detector 10 senses a grounded object 58G as illustrated 20 in FIG. 4A. The relationship of FIG. 4B assumes that the object 58G is approaching the sensor along a straight line that is perpendicular to the front plane of the sensor and intersects the transmitting electrode 12 at its center. It will be appreciated that a decrease in the distance between the grounded object 58G and the detector 10 produces a strongly decreasing detector DC output,  $V_{out}$ .

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Turning next to the sensing of partially floating or floating objects, that is, objects with intermediate or high impedance to ground, it will be appreciated that the receiver current in that case is defined by equation (2). A high impedance is defined in this context as an impedance that is much larger than the characteristic impedance of the system.

30

As illustrated in FIG. 5A, a partially floating or floating object 58F is situated within the sensing range of the detector 10. The electrically floating status of the object 58F is

represented by its connection to earth ground 75 through intermediate or high impedance  $Z_{med-high}$  34.

As the object 58F approaches, it intercepts a portion 60 of the generated electric field 56. Unlike the case for grounded objects, however, shunting of the intercepted portion directly to earth ground 75 is prevented by the intermediate or high impedance  $Z_{med-high}$  34. Instead, the field is shunted to circuit ground 70 (FIG. 1) by way of the object's capacitive coupling  $C_{OG}$  to the sensor's ground electrodes 32 and 16.

With an appropriate choice for the sizing and spacing of the sensor electrodes (such as the "bulls-eye" configuration of FIG. 2A and ranges set out in Table I), as the object 58F approaches, the object's capacitive coupling  $C_{OG}$  with ground electrodes 32 and 16 increases more quickly than the product of the object's capacitive couplings  $C_{OR}$  and  $C_{OT}$  with the receiving and transmitting electrodes 14 and 12, respectively. Accordingly, any potential increase in receiver current  $I_R$  which might otherwise result from the approach of the floating object 58F, absent the capacitive coupling  $C_{OG}$  to ground electrodes 32 and 16, is overwhelmed by the decrease in receiver current  $I_R$  caused by the shunting of charge to circuit ground 70 via the capacitive coupling  $C_{OG}$ , and the prevailing trend is a general decrease for  $I_R$ .

FIG. 5B illustrates the general relationship of object-to-electrode distance to the DC output  $V_{out}$  of the detector 10 as it senses an object 58F with intermediate or high impedance to circuit ground as illustrated in FIG. 5A. Again, it is assumed that the object 58F is approaching the sensor along a straight line that is perpendicular to the front plane of the sensor and intersects the transmitting electrode 12 at its center. As hereinbefore described, a decrease in the distance between the grounded object 58G and the detector 10 produces a prevailing decrease in the DC output  $V_{out}$ . Note however that when a partially floating or floating object has come within very close range of the electrodes, less than distance N in the graph of FIG. 5B, the decreasing trend of the DC output  $V_{out}$  may reverse itself, and the DC output  $V_{out}$  may then increase rather than decrease as the object draws still closer. With the sensor embodiment of FIG. 2A having relative proportions within the ranges set forth in Table I, and with the receiving electrode 214 having a relative outer diameter of 40 units,

distance N is about 10 units. Nonetheless, as recognized by those skilled in the art, proximity detection may still reliably occur through techniques such as the setting of an appropriate threshold receiver current, for example, such that the object will be detected well outside the range at which trend reversal occurs.

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Thus, whenever an intruding object is detected, a monotonic decrease in receiver current (at least outside a threshold distance) is produced regardless of the ground impedance of the approaching object. Consequently, the complexity of signal detector circuitry may be reduced from that of known transmit-receive detectors. Additionally, this 10 monotonic decrease promotes greater detector reliability because of the reduced likelihood that objects having intermediate earth ground impedance will escape detection.

In an alternative embodiment, the transmitting electrode and the receiving electrode may be reversed, such that the central disk comprises the receiving electrode and the 15 outermost annular ring comprises the transmitting electrode. In this case, the behavior of the proximity detector will be as described for the preferred embodiment above, provided that the receiving electrode 14 is actively maintained at circuit ground potential. When the receiving electrode 14 is not held actively at circuit ground potential, the relative proportions of the sensor electrodes for which object detection will occur may differ from 20 those indicated above for the preferred embodiment.

In alternative embodiments, the shape of the transmitting, receiving and ground electrodes may be polygonal rather than circular, such as square, hexagonal or octagonal for example. In this case, each electrode may have a different polygonal shape or some or 25 all of the electrodes may have the same polygonal shape. An exemplary arrangement is shown in FIG. 7. Again, in this case, the relative proportions of the sensor electrodes for which object detection will occur may differ from those indicated above for the preferred embodiment.

30 It should be noted that, during detector operation, the circuitry housed within the detector body 28 may produce stray electric fields 42 (FIGS. 4A and 5A) that emanate toward the sensor 20. If allowed to reach the transmitting or receiving electrodes 12 or 14,

these electric fields 42 may influence the induced receiver current  $I_R$  at the receiving electrode, potentially posing a risk to proper object detection. The risk of such stray capacitance, however, is significantly reduced as a result of the positioning of the ground electrode 16 between the detector circuitry and the receiving and transmitting electrodes 14 and 12. As illustrated in FIGS. 4A and 5A, stray electric fields 42 are intercepted by ground electrode 16 before they are able to reach the transmitting or receiving electrodes 12 or 14, and the stray electric charge is consequently shunted to circuit ground 70. Thus, the influence of stray electric fields on the receiver current  $I_R$  is diminished, and therefore the detector's susceptibility to stray capacitance is reduced.

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The risk of stray capacitance may alternatively be reduced by encasing the detector circuitry in a ground box, or through the use of a faraday shield.

15        The back plane ground electrode 16 additionally promotes directionality in object detection. As understood by persons skilled in the art, the electric field 56 generated by transmitting electrode 12 (FIGS. 4A and 5A) radiates not only towards the receiving electrode 14 but in all directions. A portion 40 of this field may in fact radiate back towards the detector circuitry. Because ground electrode 16 is interposed between the detector circuitry and the transmitting and receiving electrodes, it forms a barrier to such fields.

20        Backwards-emanating fields like the exemplary field 40 are intercepted by this barrier and shunted to circuit ground 70. As a result, the electric field generated by the transmitting electrode 12 is prevented from emanating into the region behind the back plane's ground electrode 16. Accordingly, objects approaching from behind the ground electrode 16 do not intercept the generated electric field and therefore do not affect the current  $I_R$  at the receiving electrode 14. Hence, an overall degree of directionality for the proximity detector 10 is promoted, whereby objects approaching from behind the ground electrode 16 may not be detected, yet objects approaching from other angles may be detected.

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30        While two ground electrodes 32 and 16 are preferred, it will be appreciated that alternative embodiments may utilize a different number of ground electrodes, provided that at least one is used, namely, electrode 32. In cases where the number of electrodes is greater than one, each of the electrodes is electrically coupled to circuit ground.

When the detector is in operation, the frequency and amplitude of the oscillator signal may be kept constant. Alternatively, the oscillator signal may be AM, FM, or phase modulated to allow a better signal-to-noise ratio (SNR) at the signal detector 24 (fig. 1).

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It will be recognized that, because of its ability to reliably detect objects regardless of their impedance to earth ground, the proximity detector 10 is well suited for safety applications. One such suitable safety application is the automatic switching of a personal communications device from loudspeaker or hands-free mode to handset mode. Many 10 personal communication devices, such as cellular or portable telephones, have two operating modes. The first, or handset, mode is used during normal operation when the device is held in close proximity to the user's ear, and the second, or loudspeaker, mode is used when the user wishes to carry on a conversation hands-free. Because users often toggle between these two modes, as described for example in U.S. Patent 5,729,604, there is 15 a risk that the device may accidentally be brought within close range of a user's ear while in hands-free mode, and that the user's hearing may be damaged as a result of the high volume levels associated with the hands-free mode. In this regard, a distance less than about 10 millimeters from the ear is considered to be an unsafe distance with such devices for hands-free operation.

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The present invention may significantly improve the safety of a communications device employing both handset and hands-free modes. More specifically, referencing the exemplary embodiment of FIG. 6 along with FIG. 1, the sensor 20 of a proximity detector 10 is mounted in the face plate 82 of a communications device 80. The detector circuitry 25 may be housed within the body of the device on the opposite side of the second ground electrode 16 from the transmitting and receiving electrodes 12 and 14. The sensor is oriented within the device to permit objects approaching from the face plate side of the device to be detected. In the present embodiment, the detector output is coupled to a switch 86 allowing the device to be toggled between its two operating modes. In the event that the 30 device is accidentally brought to the ear of a user 84 while in hands-free mode, the proximity detector 10, sensing the presence of the user's ear at an unsafe distance, switches the device into handset mode. The DC level output from the detector at which switching

occurs may be chosen so that switching occurs when an object is about 50 millimeters from the sensor. Thus, the risk of damage to the user's hearing may be reduced, regardless of whether the user is equivalent to a grounded object or a floating object.

5       The foregoing is merely illustrative of the principles of the invention. Those skilled in the art will be able to devise numerous arrangements which, although not explicitly shown or described herein, nevertheless embody those principles that are within the spirit and scope of the invention, as defined by the claims.

EFFECTIVE FILING DATE